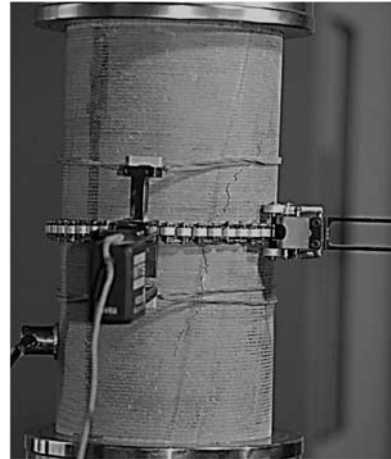


# Challenges associated with laboratory testing on Opalinus Clay, test interpretation and definition of rock mechanical properties

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ETH Zürich, Engineering Geology



Symposium Felsmechanik und Bautechnik, Zürich, 14.02.2014

## Challenges

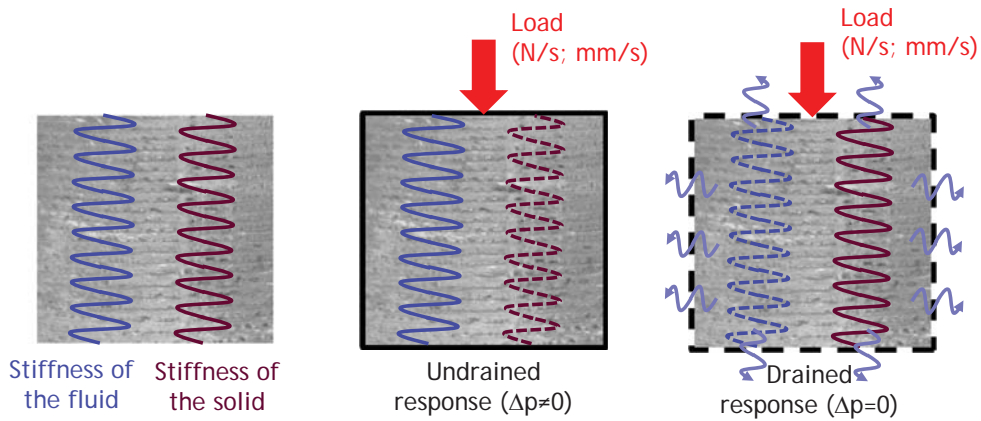
### Clay Rock Behaviour

- ✦ Initially saturated material with very low hydraulic conductivity
- ✦ Strong hydro-mechanical coupled behaviour
- ✦ Strength and stiffness anisotropy
- ✦ Sensitiveness to moisture changes
- ✦ Non-linear failure behaviour
- ✦ Time dependent deformations (consolidation, creep, viscoelasticity, clay mineral swelling)

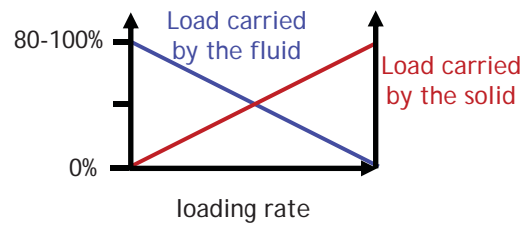
### Technical Issues

- ✦ Calibration
- ✦ Pore pressure control +
- ✦ Sufficient machine stiffness and load capacity (axial and radial pressure) +
- ✦ Extremely low loading rates
- ✦ Often long test durations
- ✦ Robustness of the equipment, temperature issues...
- ✦ Monitoring set-up → measured response versus actual specimen response

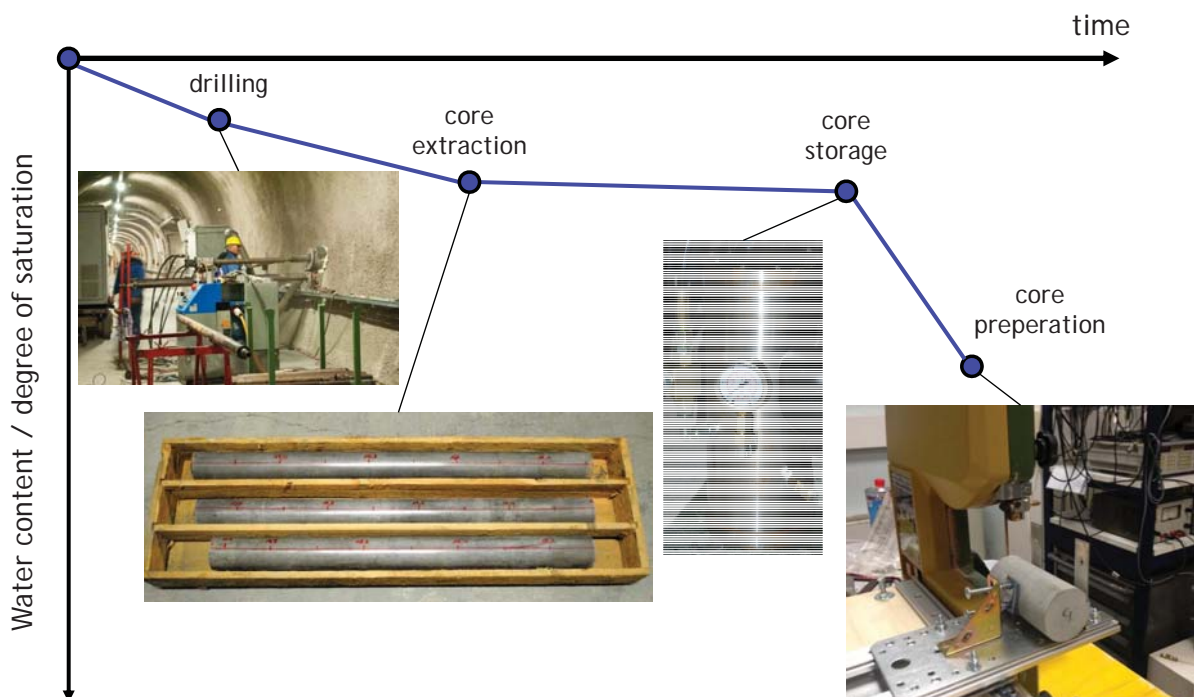
# Saturated poro-elastic medium



Undrained test: combined response of the fluid and the solid phase  
 → the two responses can be decomposed by measuring the fluid pressure during loading and the effective stress in the solid can be calculated

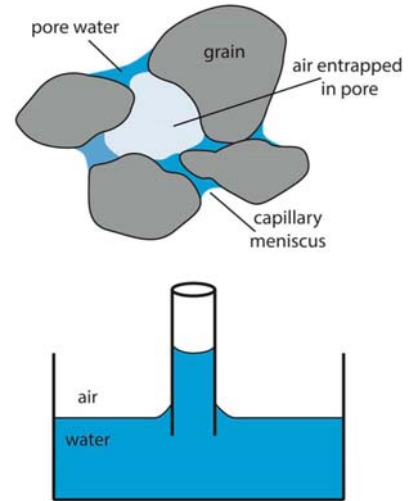
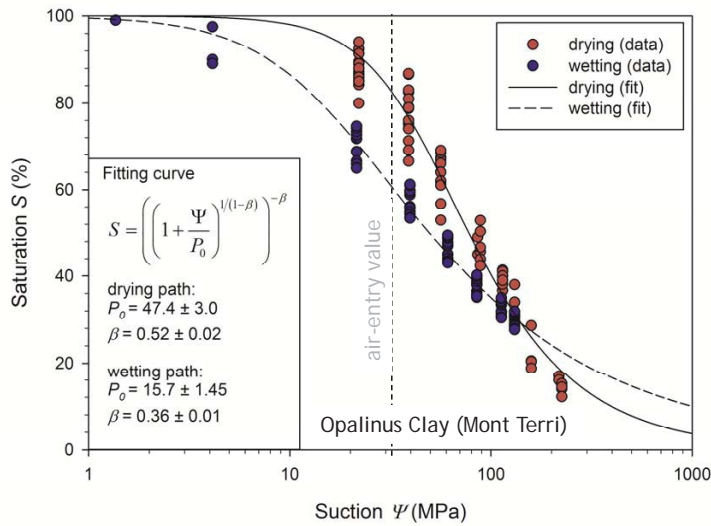


# Saturated ?



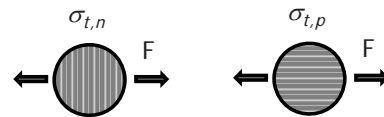
# Capillary Forces

## Water Retention Characteristics

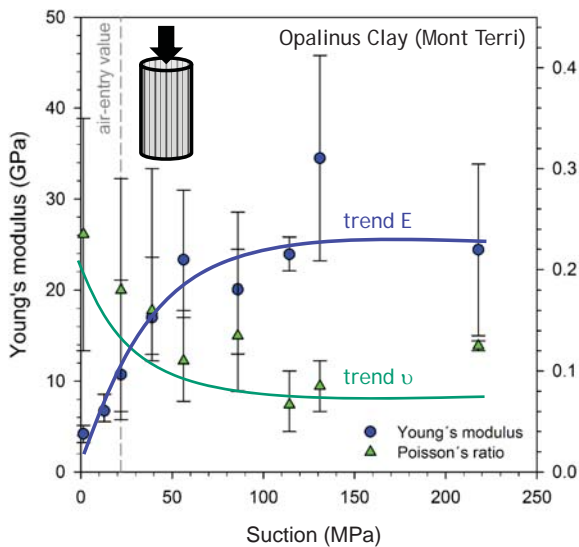


Wild et al. (in review)

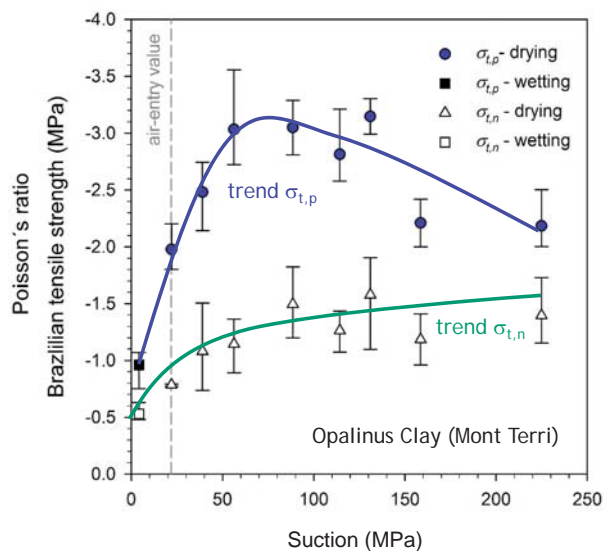
# Capillary Forces



## Elastic Properties



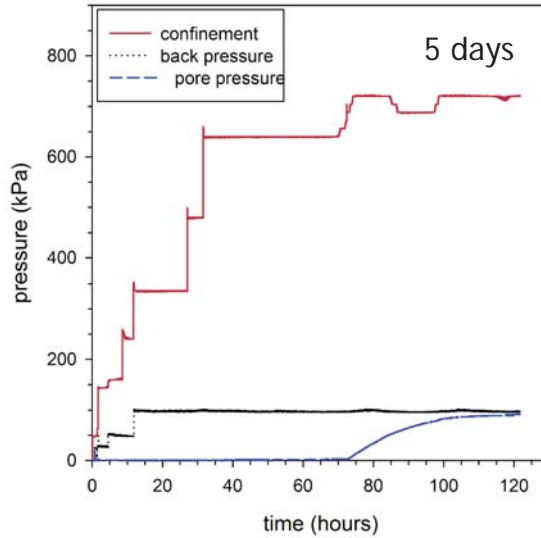
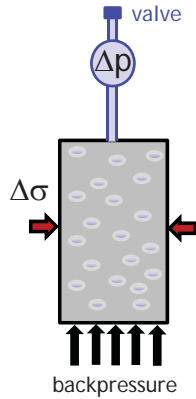
## Tensile Strength



Wild et al. (in review)

# Challenge of saturation

## Flushing Phase



The flushing phase is known to be somewhat ineffective →  
 After the flushing phase compressible air bubbles may still be present →  
 Have to be dissolved in the subsequent saturation procedure →  
 Back-Pressure Cycles

De-aired brine („Pearson-Water“)

# Challenge of saturation

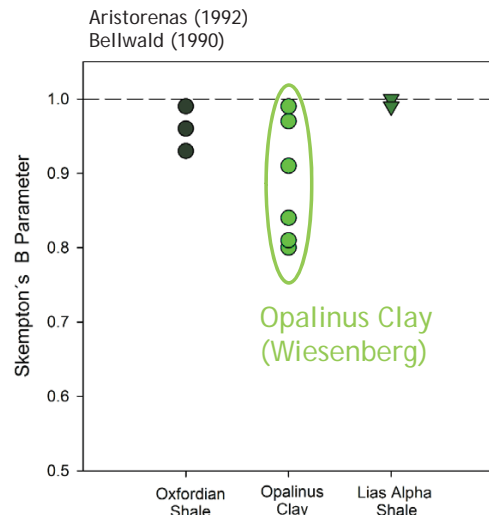
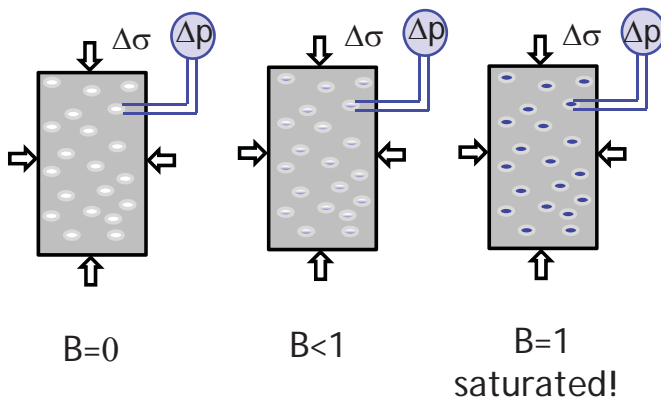
### Soils:

air: compressible  
 water: incompressible  
 solid: **incompressible**

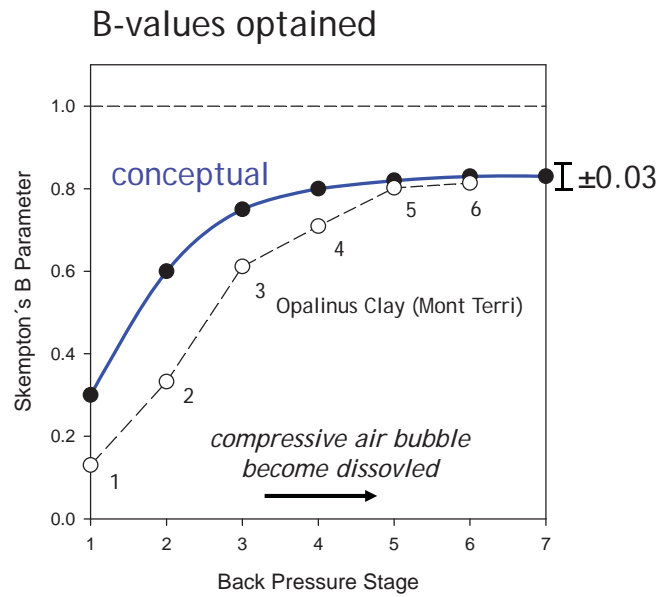
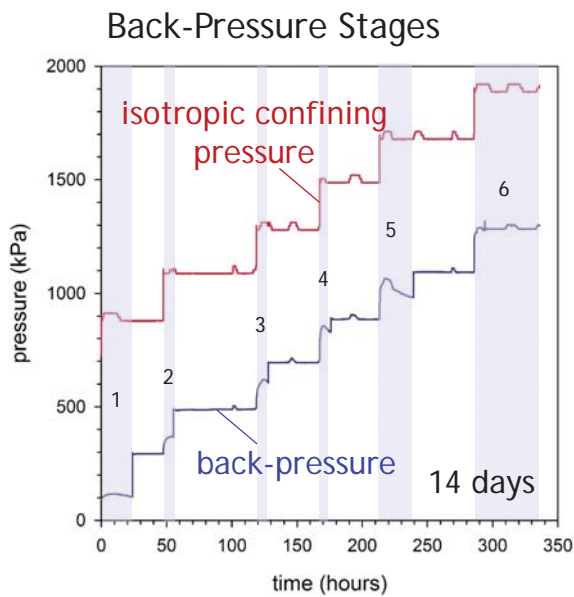
### Clay shales:

air: compressible  
 water: incompressible  
 solid: **compressible**

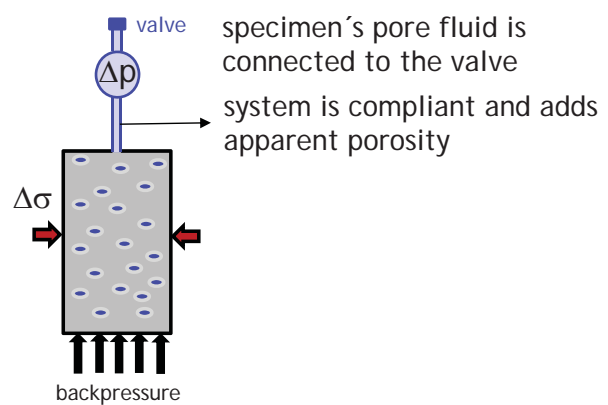
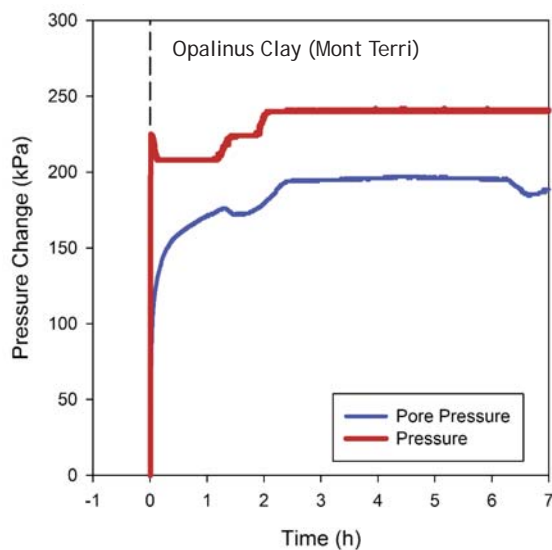
undrained isotropic loading  $B = \Delta p / \Delta \sigma$



## Challenge of saturation



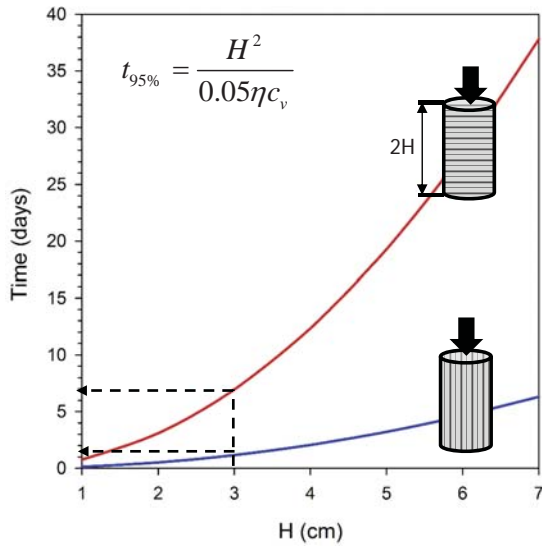
## Challenge of pore pressure measurement



→ Upon loading the pore pressure in the sample may change instantaneously, but the pore pressure measured may depend on the loading rate

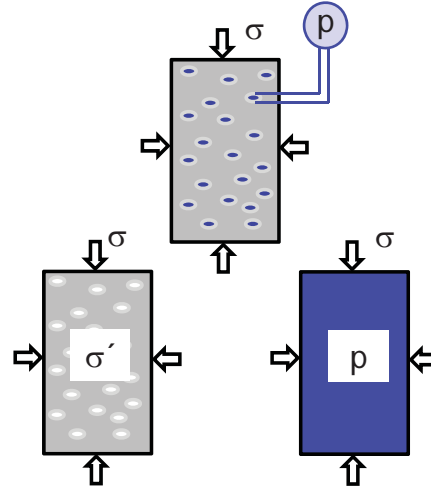
# Undrained versus drained loading

Drained compression ( $\Delta p=0$ )



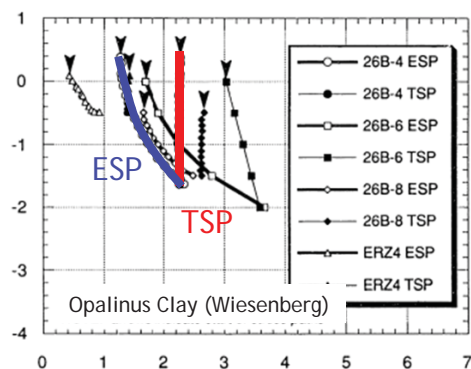
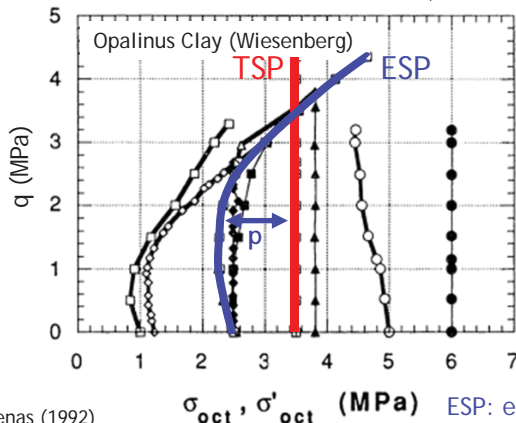
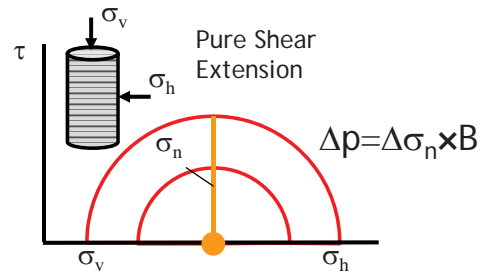
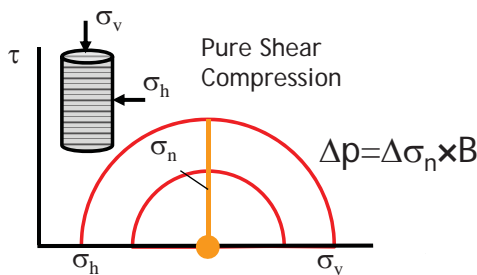
Bishop and Henkel 1957

Undrained compression ( $\Delta p \neq 0$ )



Decompose:  $\sigma' = \sigma - p$

# Aspects of undrained behaviour



Aristorenas (1992)  
Bellwald (1990)

$\sigma_{oct}, \sigma'_{oct}$  (MPa)

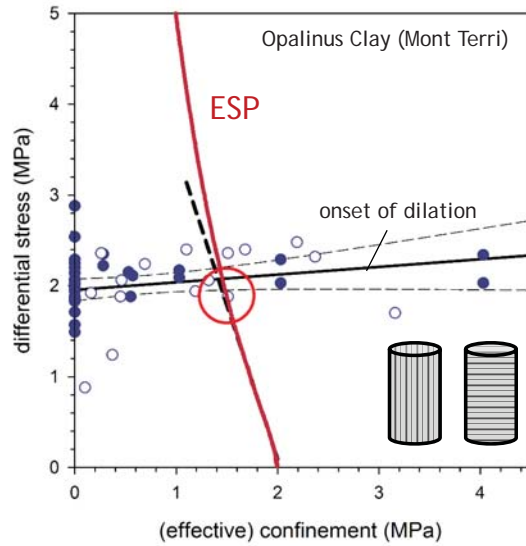
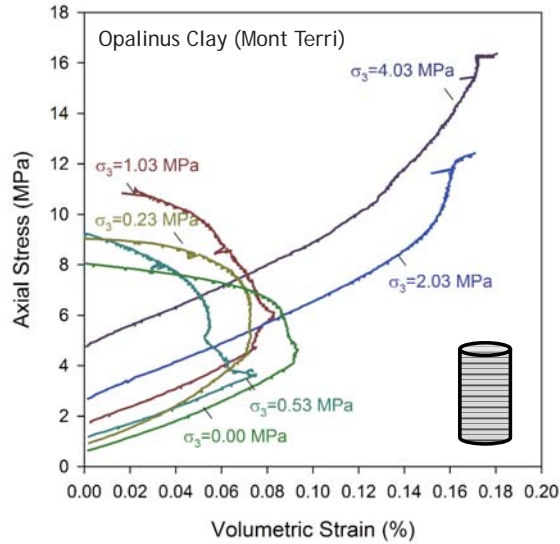
ESP: effective stress path  
TSP: total stress path

$\sigma_{oct}, \sigma'_{oct}$  (MPa)

TSP: Total  
ESP: Effect



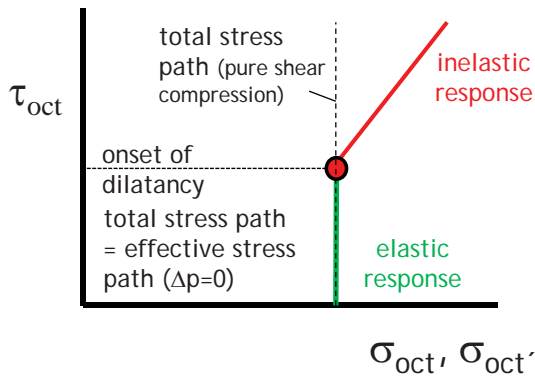
# Aspects of undrained behaviour



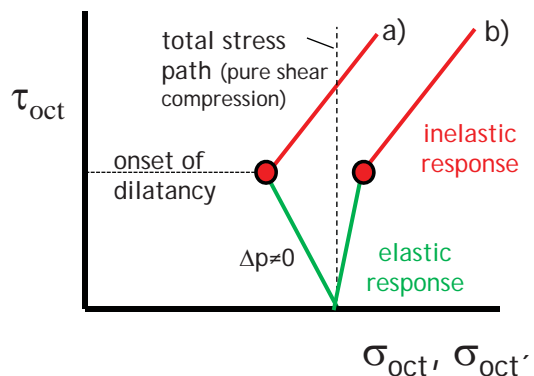
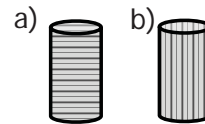
Amann et al. 2010, 2011

# Pore Pressure evolution - conceptual

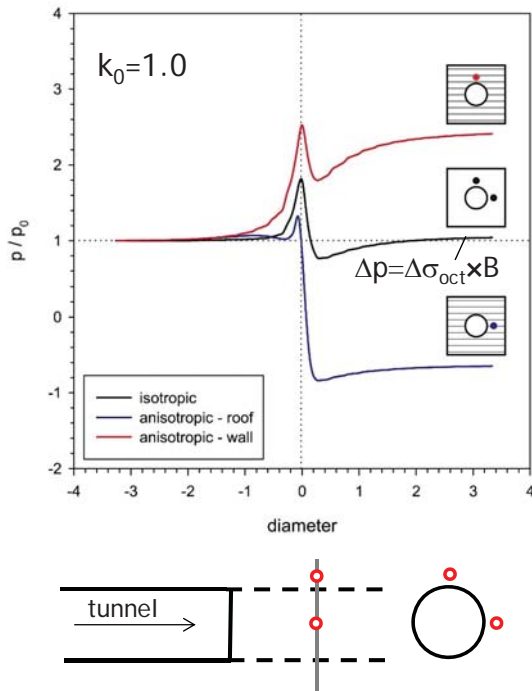
linear-elastic, brittle material  
 $\Delta p = \Delta \sigma_{oct,n} \times B \rightarrow (\epsilon_v = 0)$



transversal-isotropic, brittle material



# Elastic behaviour and simplifications

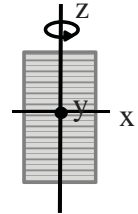


For describing a transversal isotropic poro-elastic material, 7 independent variables are required:

$$E_{x,u}, E_{z,u}, \nu_{yx,u}, \nu_{zx,u}, G_{zx}, B_x, B_z$$

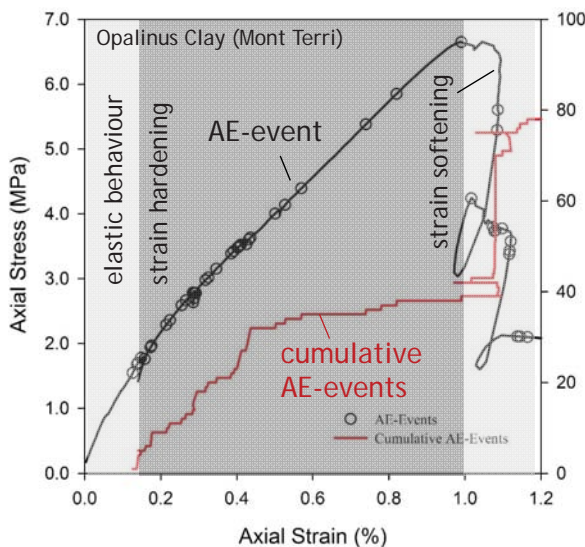
The cross shear modulus  $G_{zx}$  cannot be determined from triaxial tests on cylindrical specimens

The two Skempton's Parameter are additionally needed to calculate effective (drained) elastic properties

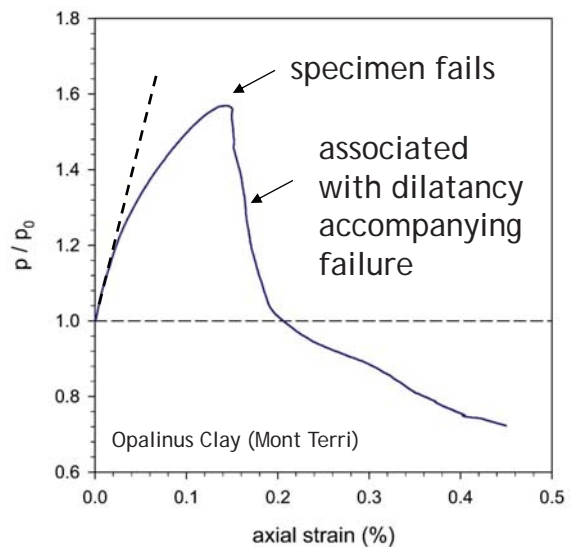


# Aspects of undrained behaviour

non-linear stress-strain response



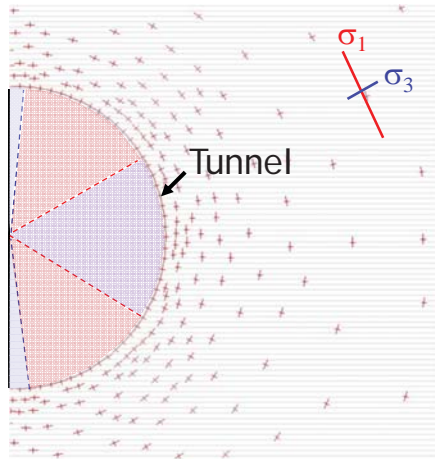
pre- and post-failure  $\Delta p$



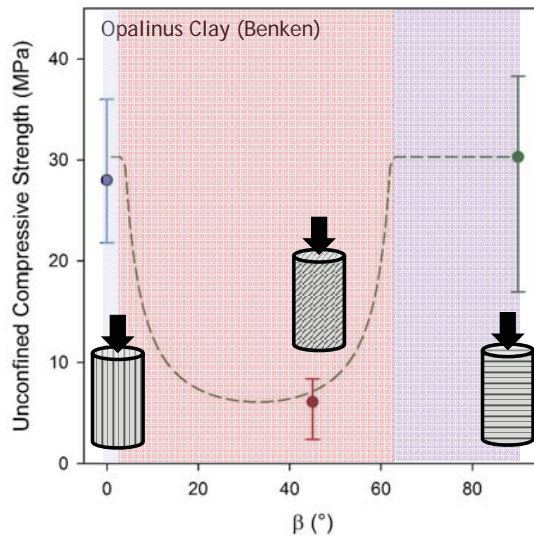


# Anisotropic Strength

## Stress trajectories

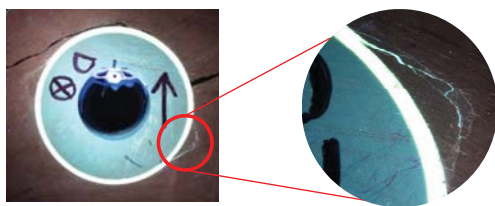


## Anisotropy in strength

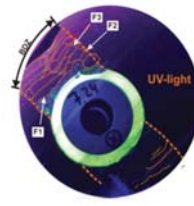


NAB 08-48, NIB 99-39, NIB 99-36b

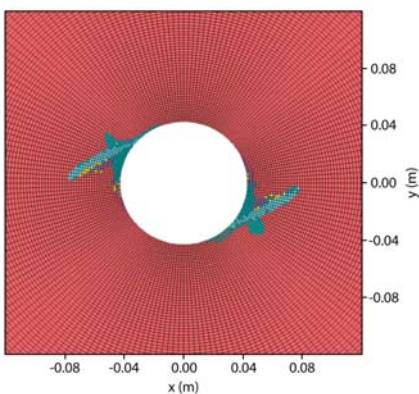
# Calibration of numerical models



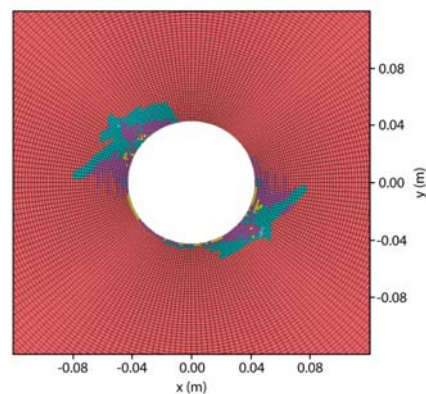
19 h after drilling  
(Kupferschmied 2013)



2 y after drilling  
(Jaeggi et al. 2010)



undrained response



30 days of pore pressure dissipation

## Summary

- ⊕ Challenges are not only associated with the material behaviour  
→ requirements on the testing device combining pore pressure measurement, testing stress states close to the in-situ state, and high control on loading rates
- ⊕ Mathematical models demand for effective rock properties which can be obtained by 1) drained testing ( $\Delta p=0$ ; *assure saturation, extremely slow loading rates, superimposed behaviors, temperature effects*) or 2) undrained testing ( $\Delta p \neq 0$ ) with reliable measurements of the pore pressure response (*assure saturation, system response, effective properties are calculated*)
- ⊕ Challenge to fully quantify effective parameters of a transversal isotropic elastic, brittle/non-linear failing anisotropic solid

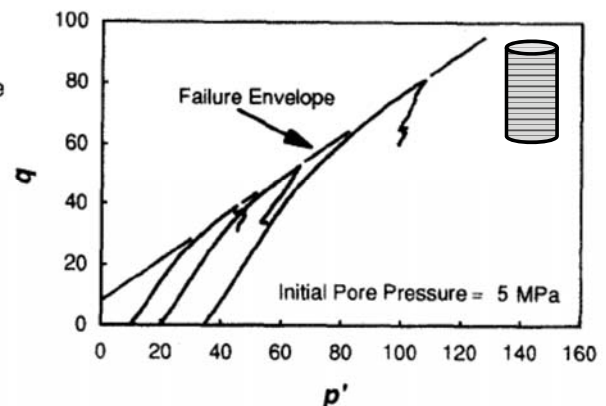
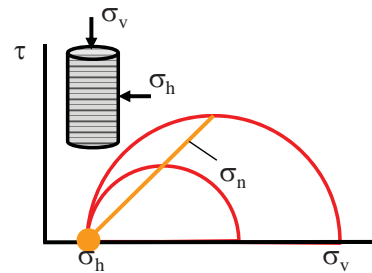
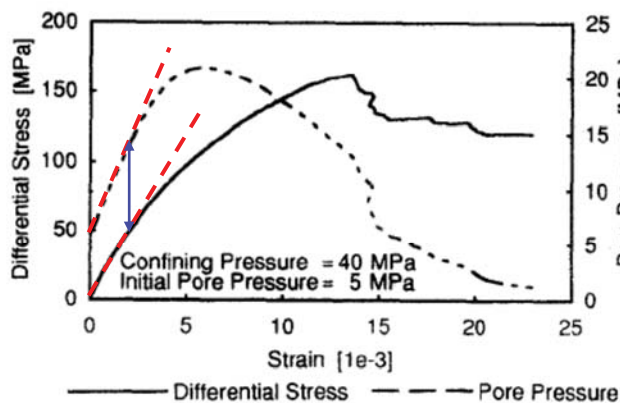
## Zusammenfassung

- ⊕ Herausforderungen nicht nur bezüglich des Materialverhaltens  
→ Anforderungen an das Testgerät, d.h. Porendruck-Messung, Test unter in-situ Spannungsbedingungen und sehr gute Kontrolle der Belastungsraten
- ⊕ Mathematische Modelle verlangen nach effektiven Felseigenschaften durch 1) drainierte Tests ( $\Delta p=0$ ; *Probensättigung, sehr geringe Belastungsraten, überlagernde Prozesse, Temperatureffekte*) oder 2) undrainierte Tests ( $\Delta p \neq 0$ ) mit belastbarer Messung des Porendrucks (*Probensättigung, Systemverhalten, effektive Eigenschaften werden rechnerisch ermittelt*)
- ⊕ Herausforderung die effektiven Parameter eines transversal isotropen elastischen, spröde/nicht-linear versagenden, anisotropen Materials zu quantifizieren

# Thank you for the attention

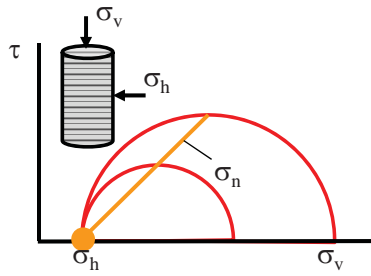
ENSI (Dr. Erik Frank)  
Linda Wymann  
Sebastian Zimmer  
Reto Thöny  
Prof. Dr. Derek Martin

## Undrained loading

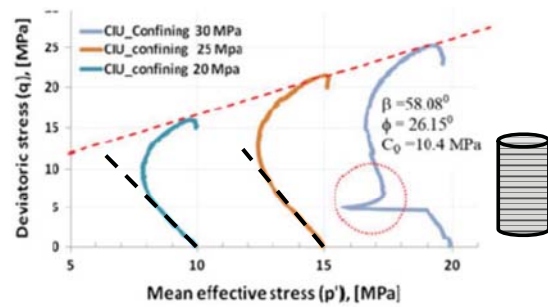
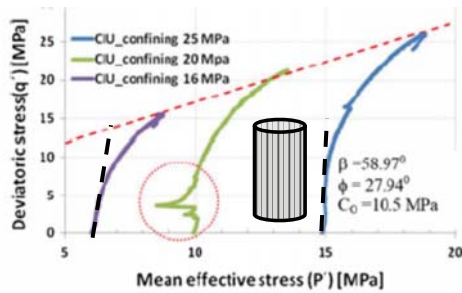


Failure envelope can be described as linear although the stress path deviates from linearity when approaching failure

# Undrained loading

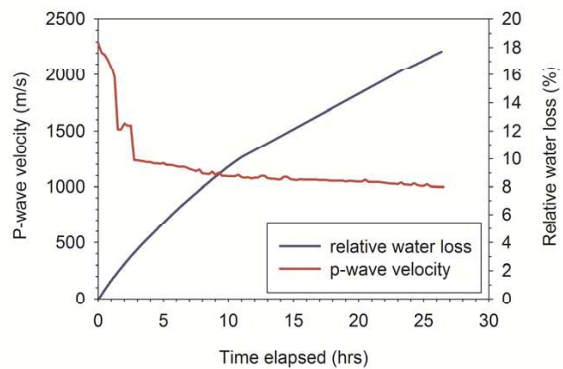
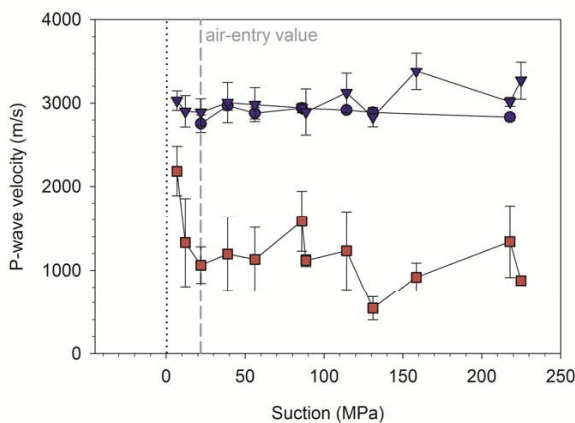


Failure envelope can be described as linear although the stress path deviates from linearity when approaching failure



Islam & Skalle (2013)

# Capillary Forces



Wild et al. (2014)