



# Rock mass behavior during excavations in the Mont Terri Underground Rock Laboratory

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Fabrice Burrus (Groupe Grands Travaux, Delémont)  
Erik Frank (ENSI, Brugg)



## Structure of the talk

- Excavation techniques
- Lining
- Rock mass behaviour during and after the excavation
- Conclusions

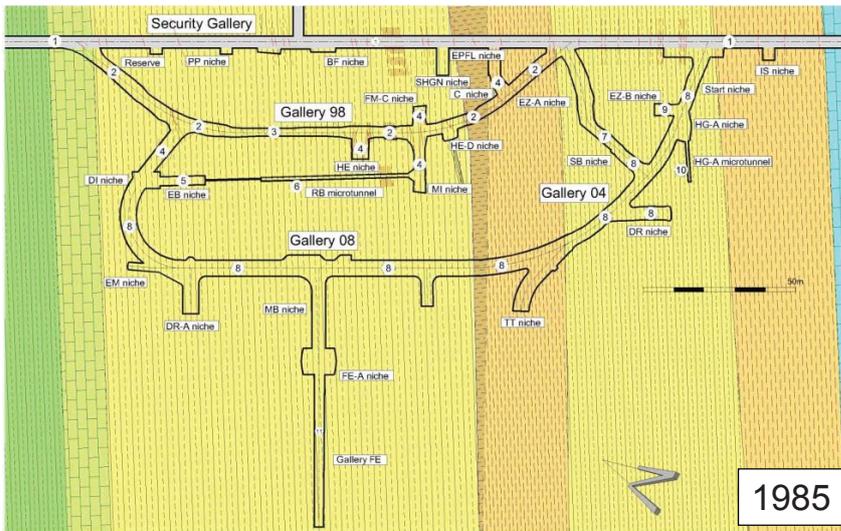


# Excavation techniques



## Mont Terri Project

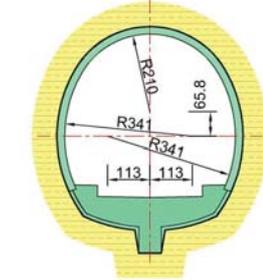
Profile type 1



### GEOLOGICAL LEGEND

Opalinus Clay	sandy facies	Jurensis Marls	Lower Dogger
	sandy, carbonate-rich facies	Posidonia shales	Singles fault
	shaly facies	Obtusus clay + Obtusus layers	Main fault

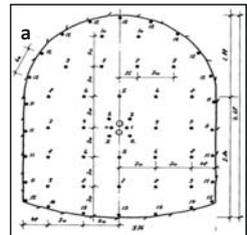
### EXCAVATION TECHNIQUES



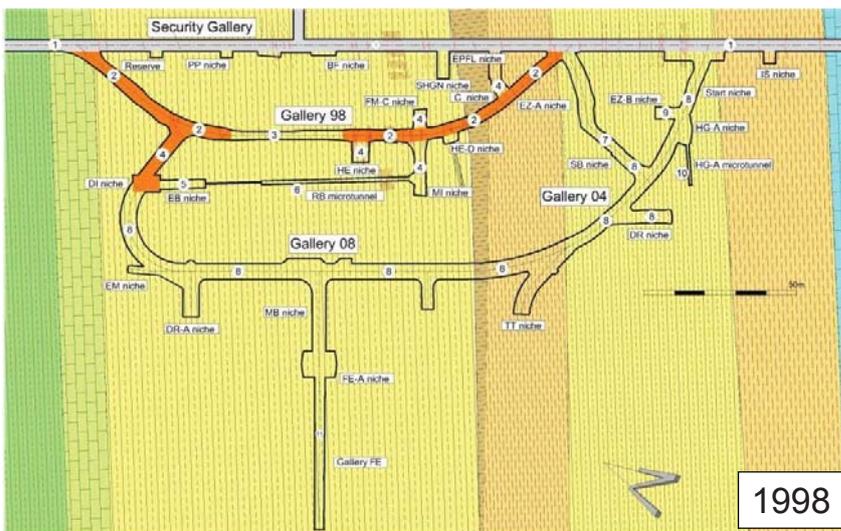
# Excavation techniques: drill and blast



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Profile type 2 (variable geometry)

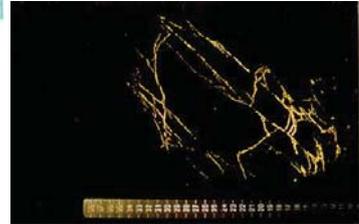
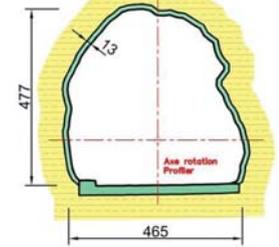


### GEOLOGICAL LEGEND

Opalinus Clay	sandy facies	Jurensis Marls	Lower Dogger
	sandy, carbonate-rich facies	Posidonia shales	Singles fault
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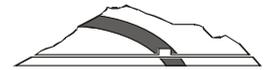
### EXCAVATION TECHNIQUES

Drill and blast

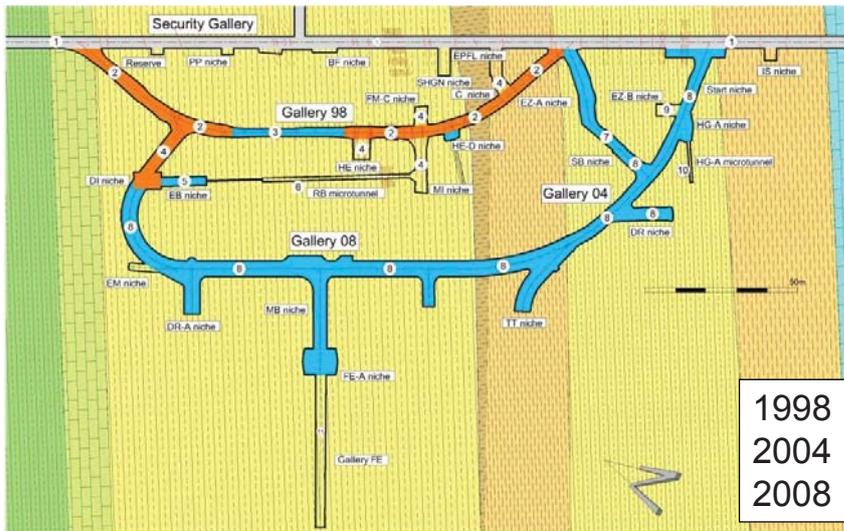




# Excavation techniques: road header



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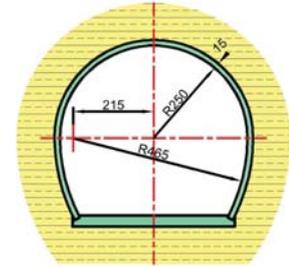
### GEOLOGICAL LEGEND

- Opalinus Clay
  - sandy facies
  - sandy, carbonate-rich facies
  - shaly facies

### EXCAVATION TECHNIQUES

- Jurensis Marls
- Posidonia shales
- Obtusus clay + Obtusus layers
- Lower Dogger
- Singles fault
- Main fault
- Drill and blast
- Road header

Profile types 3, 7 and 8



# Excavation techniques: hydraulic hammer



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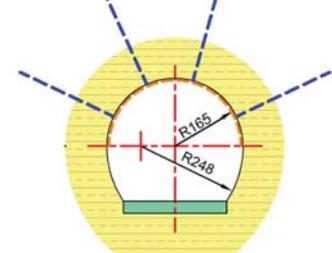
### GEOLOGICAL LEGEND

- Opalinus Clay
  - sandy facies
  - sandy, carbonate-rich facies
  - shaly facies

### EXCAVATION TECHNIQUES

- Jurensis Marls
- Posidonia shales
- Obtusus clay + Obtusus layers
- Lower Dogger
- Singles fault
- Main fault
- Drill and blast
- Road header
- Pneumatic hammer

Profile type 4

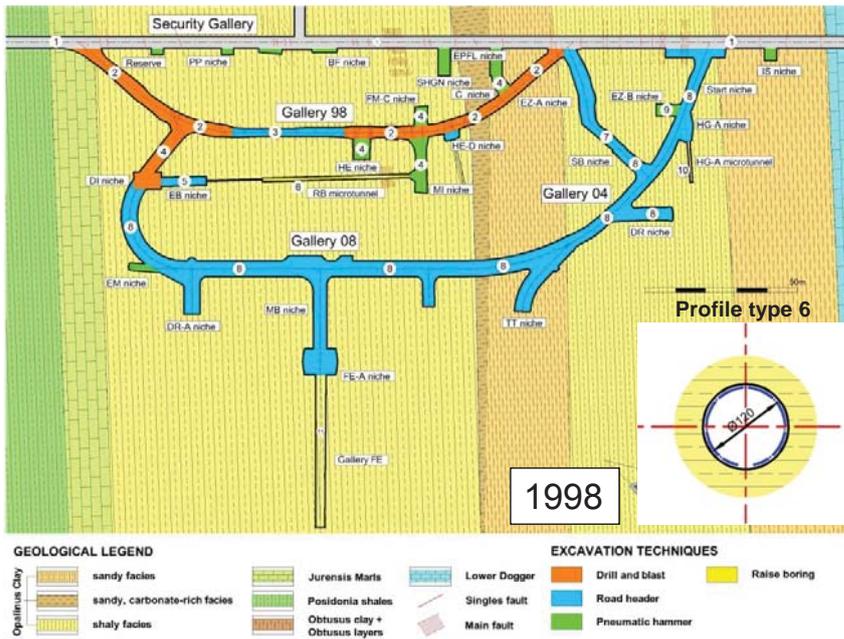




# Excavation techniques: raise boring



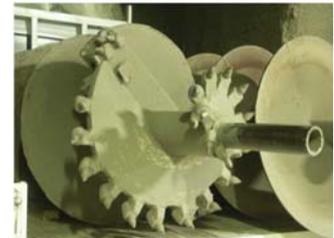
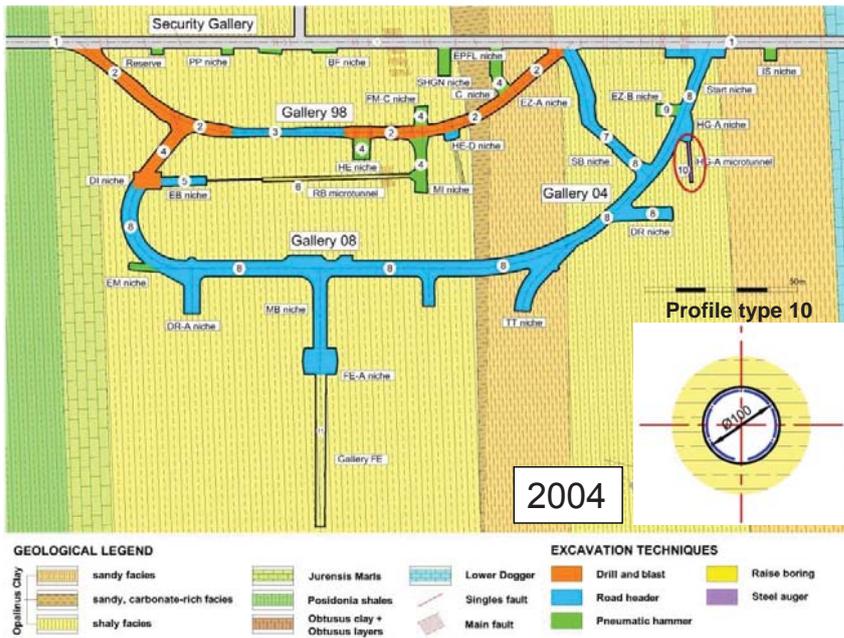
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# Excavation techniques: steel auger

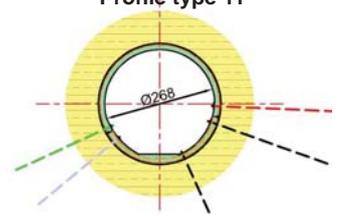


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# Excavation techniques: hydraulic hammer and road header



### GEOLOGICAL LEGEND

- Opalinus Clay: sandy facies, sandy, carbonate-rich facies, shaly facies
- Jurensis Marls
- Posidonia shales
- Obtusus clay + Obtusus layers

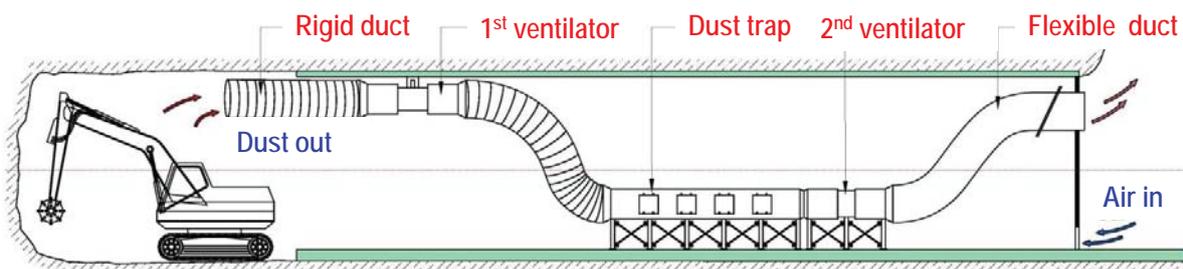
### EXCAVATION TECHNIQUES

- Lower Dogger
- Singles fault
- Main fault
- Drill and blast
- Road header
- Pneumatic hammer
- Raise boring
- Steel auger
- Pneumatic hammer and road header

2012



# Excavation techniques: dust evacuation





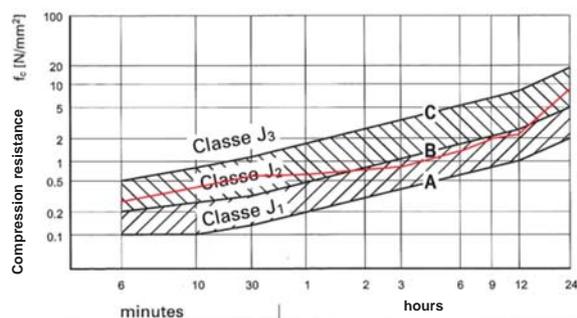
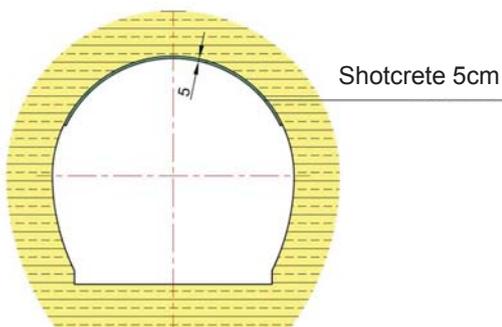
## Excavation techniques: experience



- **No water:** wet excavation and drilling with water cause deformation due to swelling
- **Road header:** best technique in terms of excavation progress, precise profiling and costs
- **Dust evacuation:** closed system with dust trap and 2 ventilators. Suva conditions fulfilled.

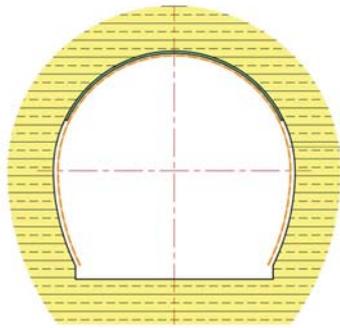


## Lining: first layer of shotcrete (with fibres)





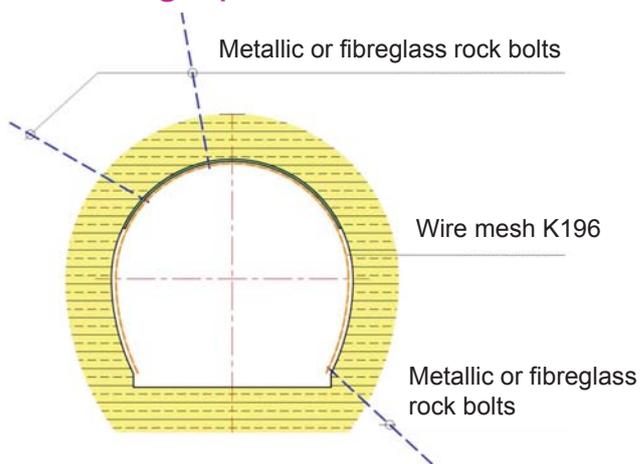
# Lining: steel wire meshes



Wire mesh K196



# Lining-optional: metallic or fibreglass rock bolts

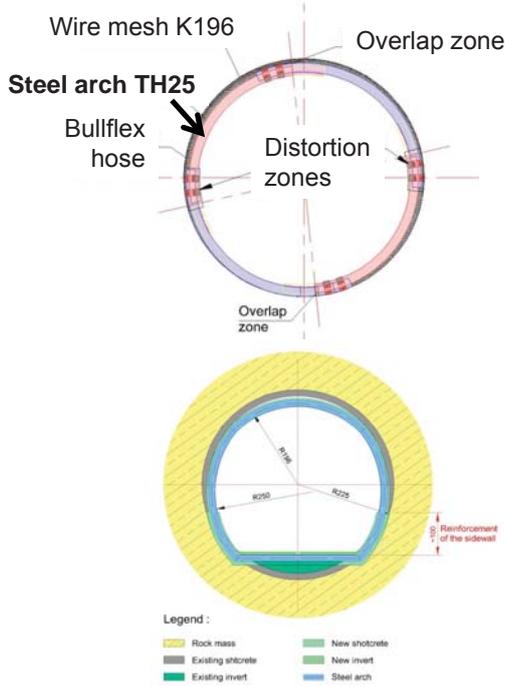




## Lining-optional: steel arches



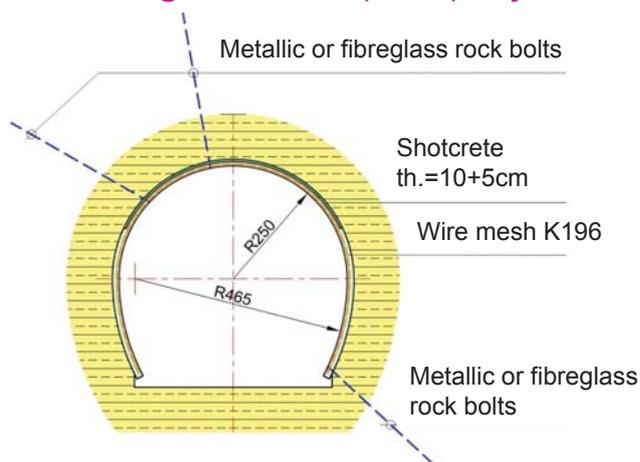
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## Lining: second (final) layer of shotcrete

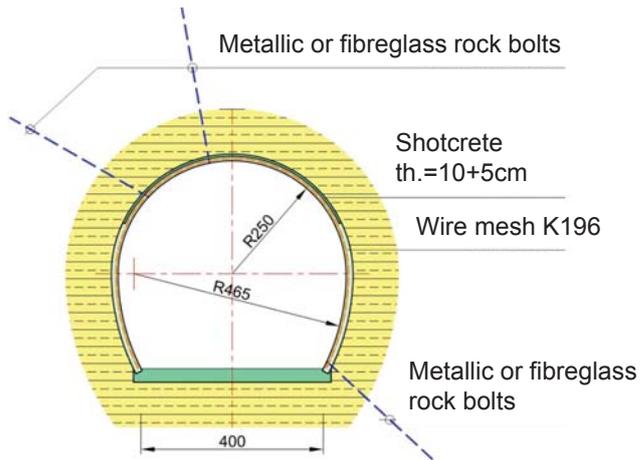


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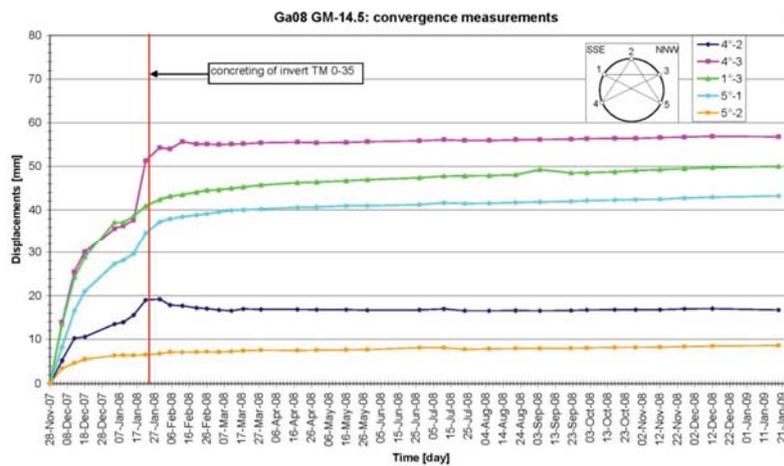




## Lining: invert

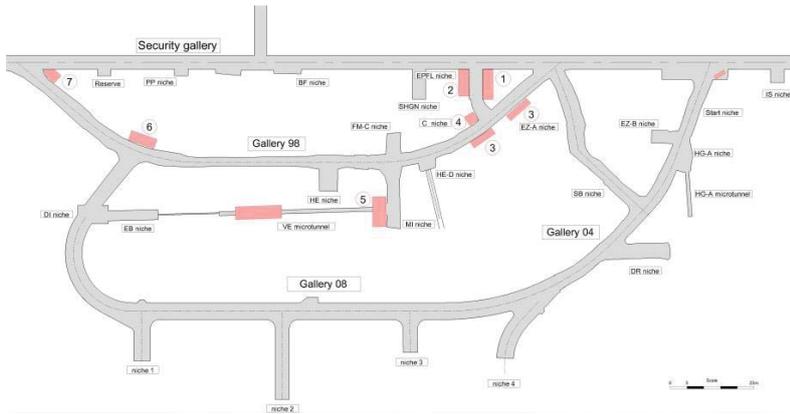


## Lining: convergence measurements



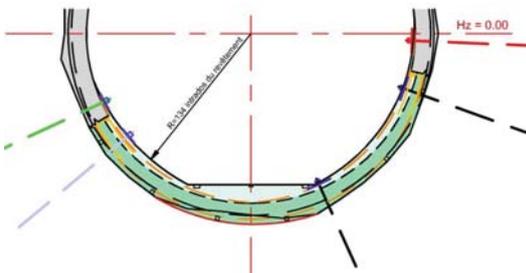


## Lining: renovation



## Lining: renovation (Gallery FE)

- Removal of liner at the invert
- 1<sup>st</sup> shotcrete layer and Installation of steel wire meshes
- Installation of new rock bolts
- 2<sup>nd</sup> shotcrete layer





- **Protection of Opalinus Clay:** lining avoids desaturation of Opalinus Clay (shrinkage, desiccation cracks)
- **Convergence confinement method:** final lining is not placed immediately after excavation. Limited convergences are allowed.
- **Safety and stability:**
  - short-term safety (accessibility for miners, SUVA conditions)
  - long-term safety (stability of galleries)
  - monitoring & supervision of convergences (monthly-1/2 year)
  - localised shotcrete renovation (after 10 - max. 20 years)



### Role of

- Anisotropy
- Tectonic Faults
- Excavation Damaged Zone (EDZ)

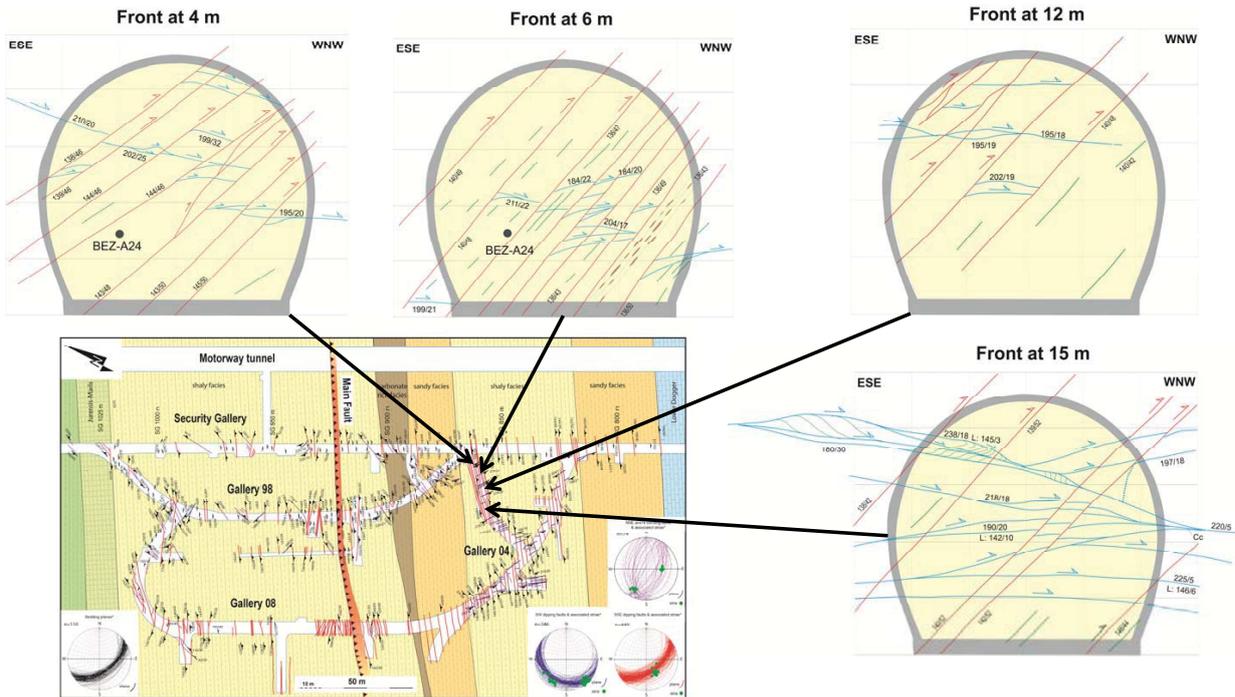




# Rock mass behaviour: Example anisotropy induced breakout (1 of 3)



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# Rock mass behaviour: Example anisotropy induced breakout (2 of 3)



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Photos: K. Schuster, BGR

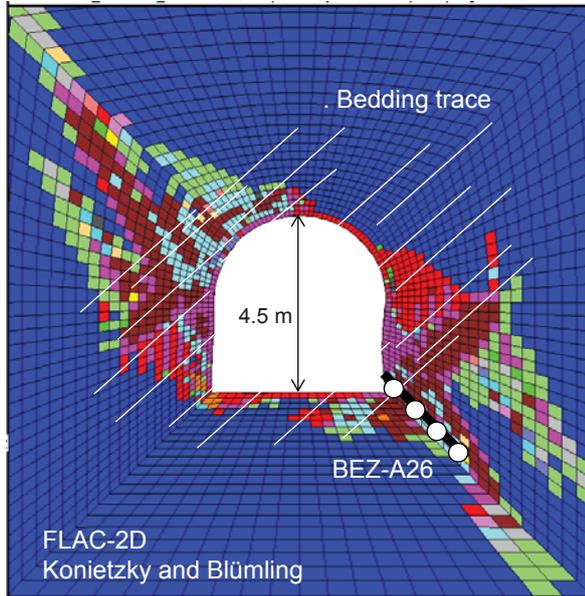


# Rock mass behaviour: Example anisotropy induced breakout (3 of 3)

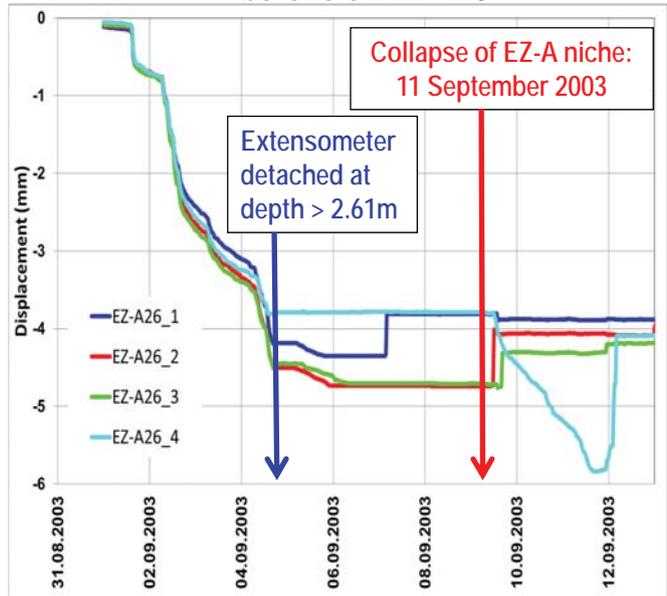


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**Modelling**  
Reduction of strength and stiffness  
Zone of several tunnel diameters



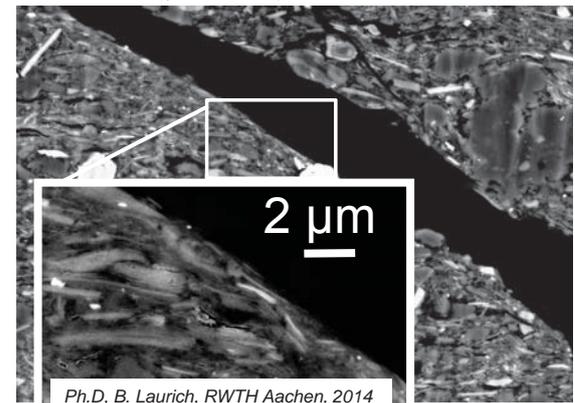
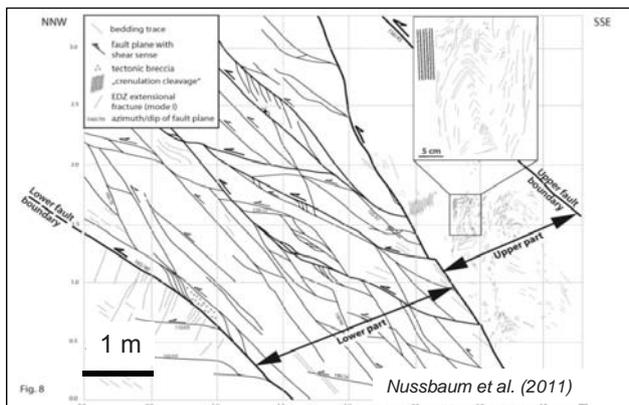
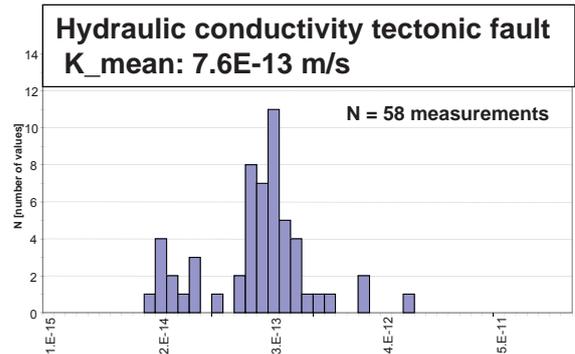
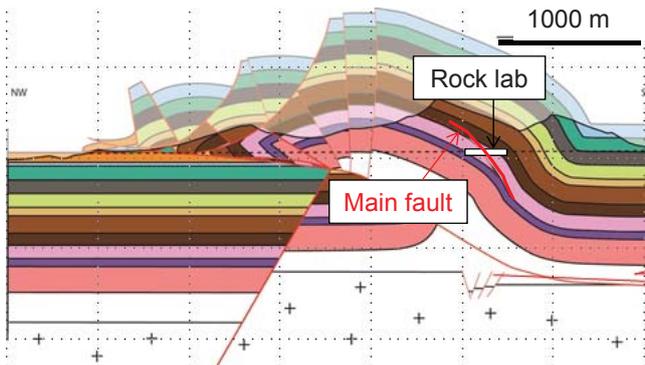
Confirmed by 4-point extensometer which was detached 1 week before collapse in borehole BEZ-A26



# Rock mass behaviour: Tectonic Fault



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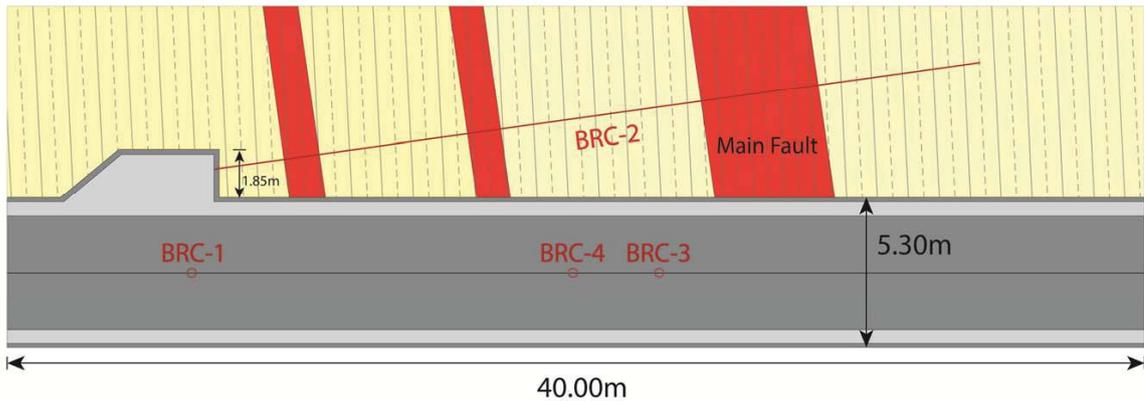


Ph.D. B. Laurich, RWTH Aachen, 2014

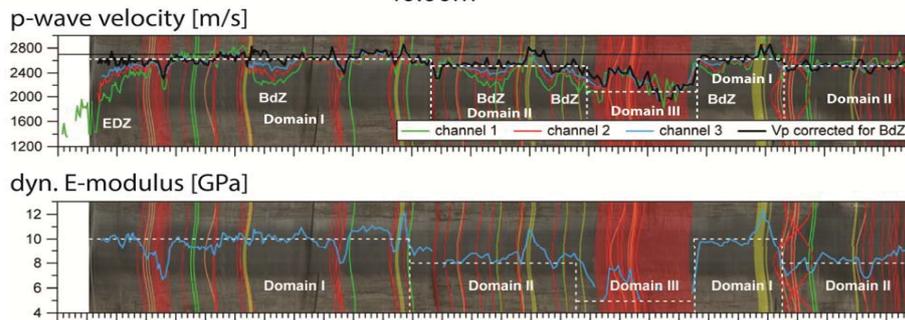


# Rock mass behaviour: Tectonic Fault

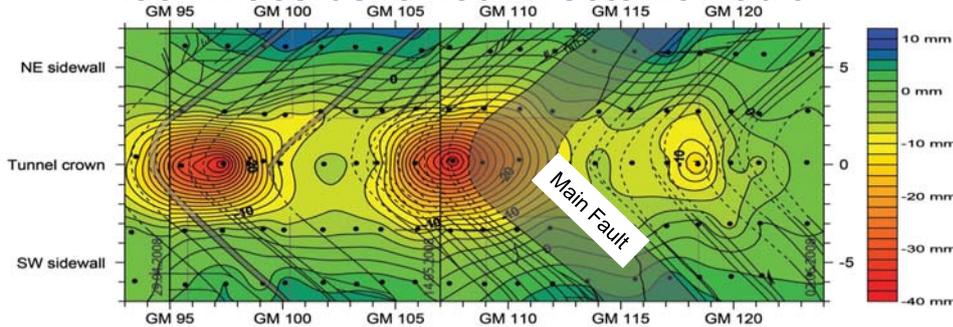
## Reduced seismic velocity & E-modulus



Seismic data from K. Schuster (BGR) in Ph.D, R. Thoeny, (ETH), 2013

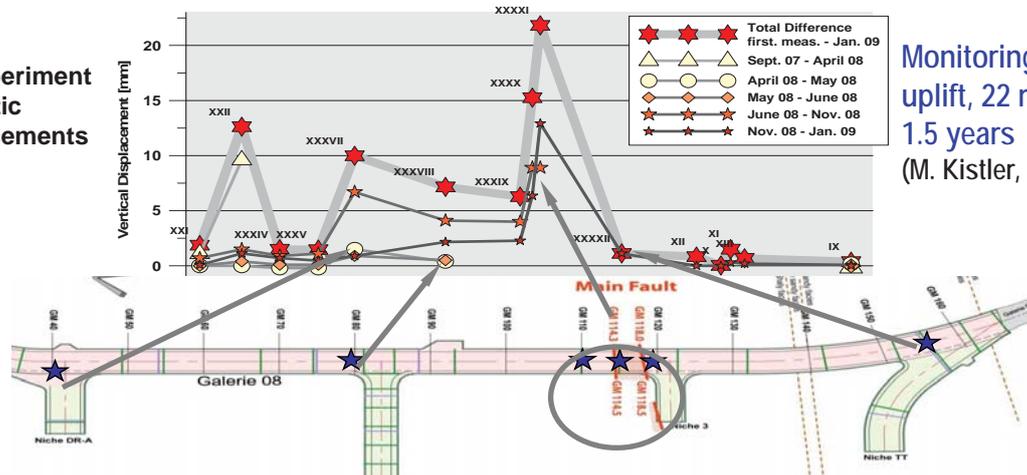


# Rock mass behaviour: Tectonic Fault



Cumulative vertical displacements at crown up to 40 mm  
Ph.D. R. Thoeny, ETH, 2013.

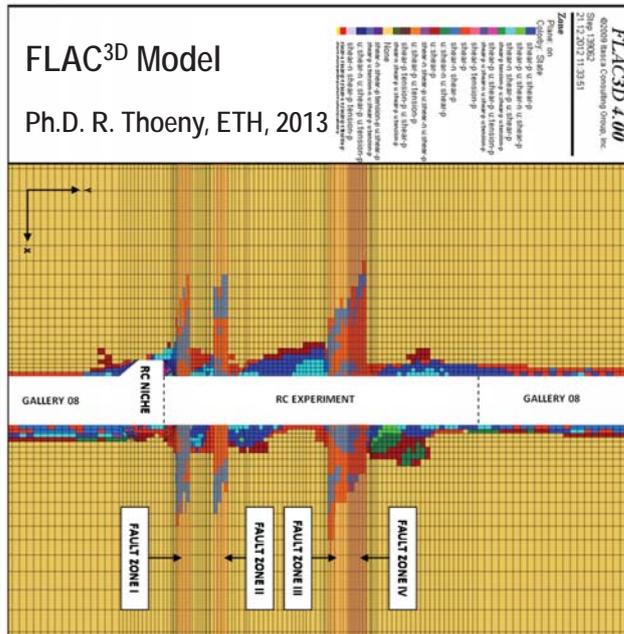
RC experiment  
Geodetic displacements



Monitoring of invert uplift, 22 mm over 1.5 years  
(M. Kistler, swisstopo)



## Rock mass behaviour: Main Fault Integration of results, conclusion

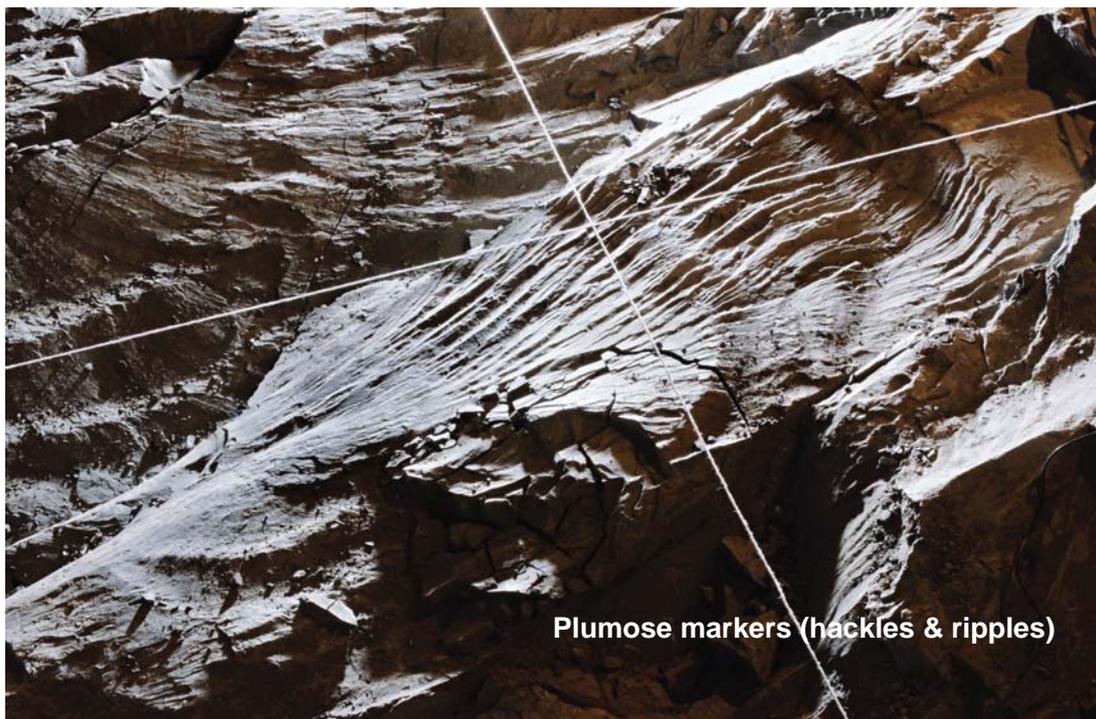


- Heterogeneous system (stiffness contrast between faults and matrix)
- Bedding- and fault-parallel shear displacements ahead of excavation front, vertical displacements at crown and invert
- Extension fracturing in sidewalls (EDZ fractures)
- Extent of plastic deformations: 2-3 tunnel diameters

Stress tensor of Martin and Lanyon (2003) was used

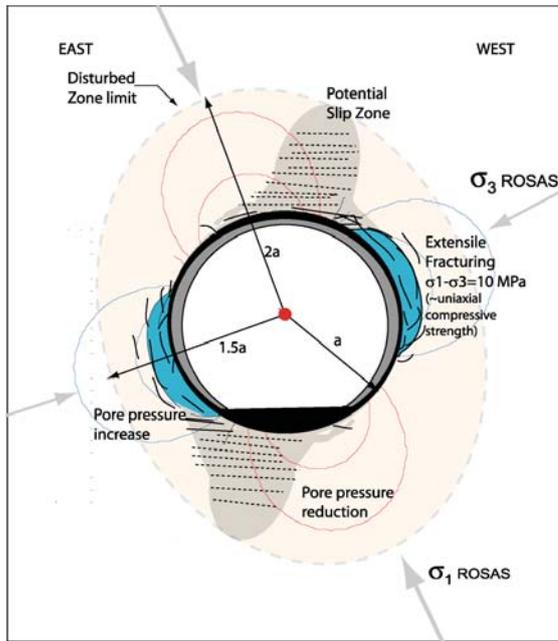


## Rock mass behaviour: Excavation damaged zone (EDZ)

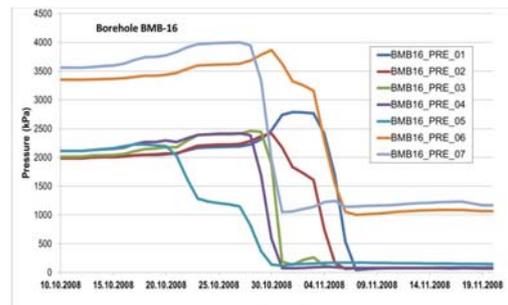
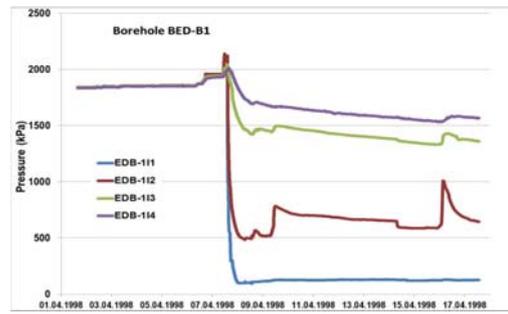




# Rock mass behaviour: Conceptual model of EDZ (HM-coupling)



Martin, D.D. and Lanyon, G.W., 2001

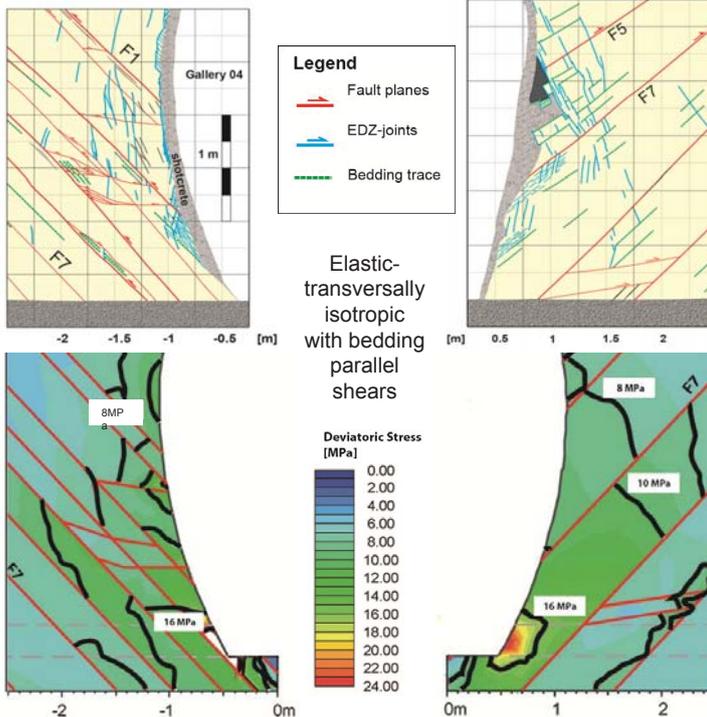


# Rock mass behaviour: EDZ



Niche EZ-B, east wall

west wall



Ph.D, S. Yong, (ETH), 2011; Yong et al., 2010

Small scale mapping

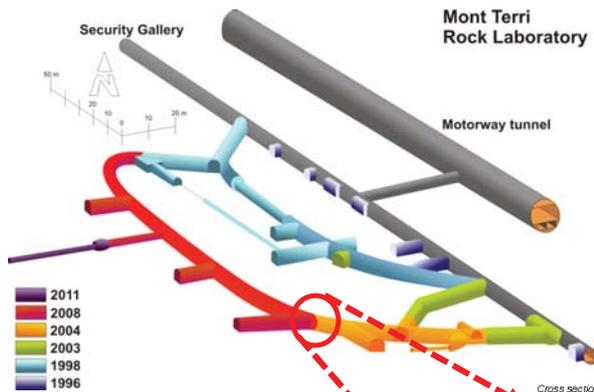
- EDZ-fracture termination near tectonic fault planes
- Tectonic fault reactivation (fault plane parallel shear)

Modelling (3DEC)

- Matrix: extension fractures (deviatoric stress > 8 MPa)
- Fault: tectonic shear zones are reactivated (fault plane parallel shear)

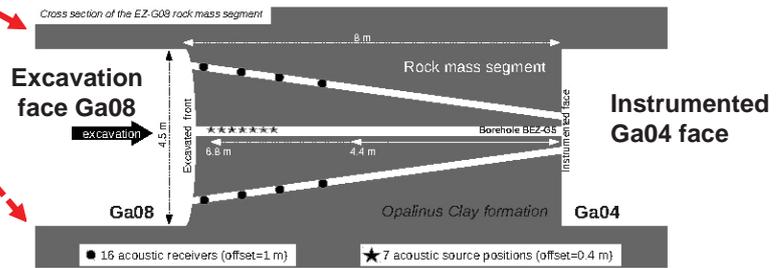
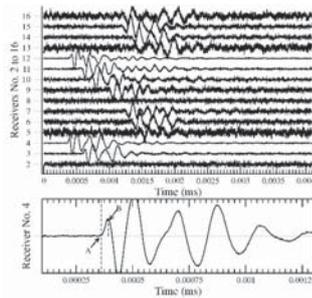


# Rock mass behaviour: EDZ

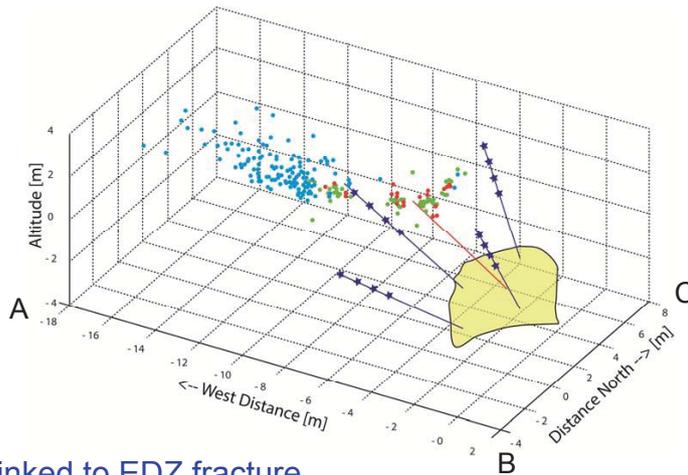


## Monitoring of the EDZ with active and passive geophysical methods: the EZ-G experiment

Ga04 face: 4-years old EDZ  
 Advancing Ga08 face: newly formed EDZ

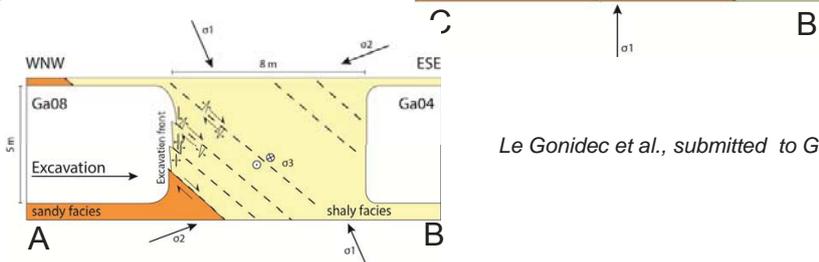


# Rock mass behaviour: EDZ Locations of micro-seismic events (SE)



- 56'446 events detected
- 278 processed true events
- 11 July 2008 (191 events)
- 12 July 2008 (71 events)
- 13 July 2008 (16 events)

- SE linked to EDZ fracture formation
- Fractures formed simultaneously to excavation
- Fractures concentrated to shaly facies; sandy facies aseismic?

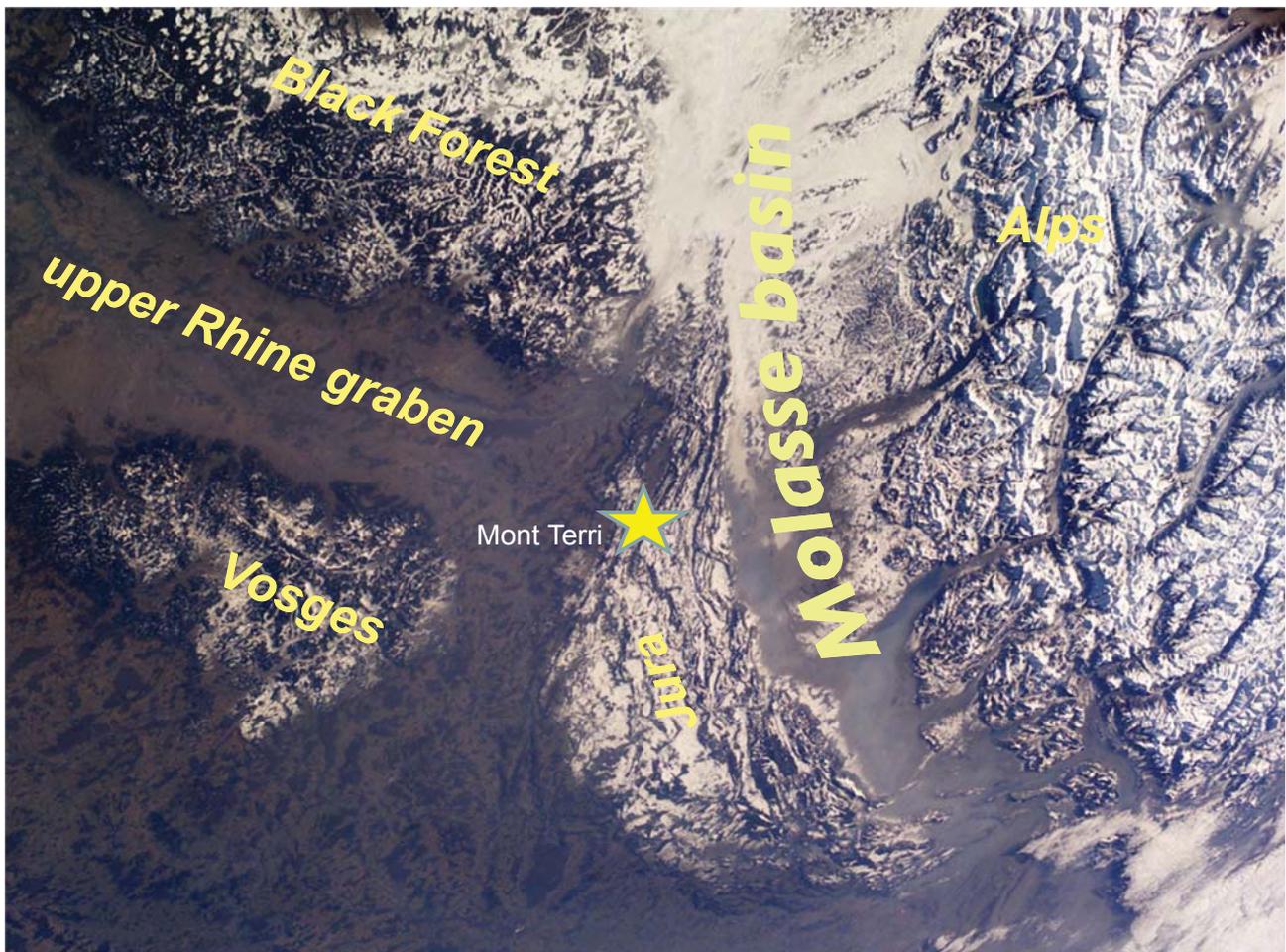


Le Gonidec et al., submitted to GJI



Which results from Mont Terri can be transferred to a future repository for high level waste in the Opalinus Clay?

- Role of anisotropy: partly transferable (rotation of  $45^\circ$ ). Enhanced convergences and breakouts at tunnel roof and floor. Not transferable is the stress field.
- Role of tectonic faults: partly transferable. Clearly lower fault frequency at potential future sites (*Mont Terri = worst case, tectonically active faults?*). However fault zones at future repository sites cannot be excluded
- Role of EDZ: partly transferable. Clearly more pronounced than at Mont Terri (Mont Terri: 300 m, future site for HLW between 400 and 900 m)





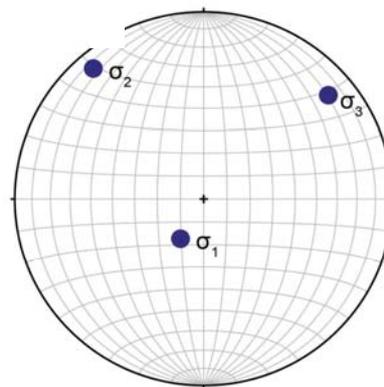
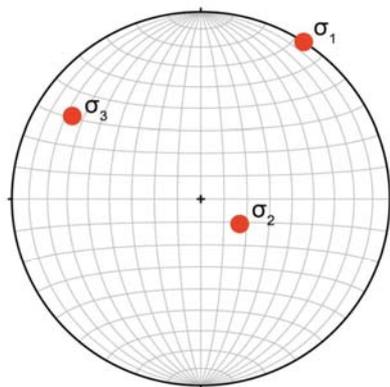
## Which facies to be selected for a repository in the Opalinus Clay?

- Sandy facies is recommended (higher UCS, higher elastic moduli). Higher short- and long-term safety, better (cheaper) maintenance.
- Shaly facies at Mont Terri in a depth of 300 m is a proxy for the sandy facies in a future repository in a depth of 600-900 m.



Remote stresses Hauptrogenstein

Remote stress Opalinus Clay in rock lab

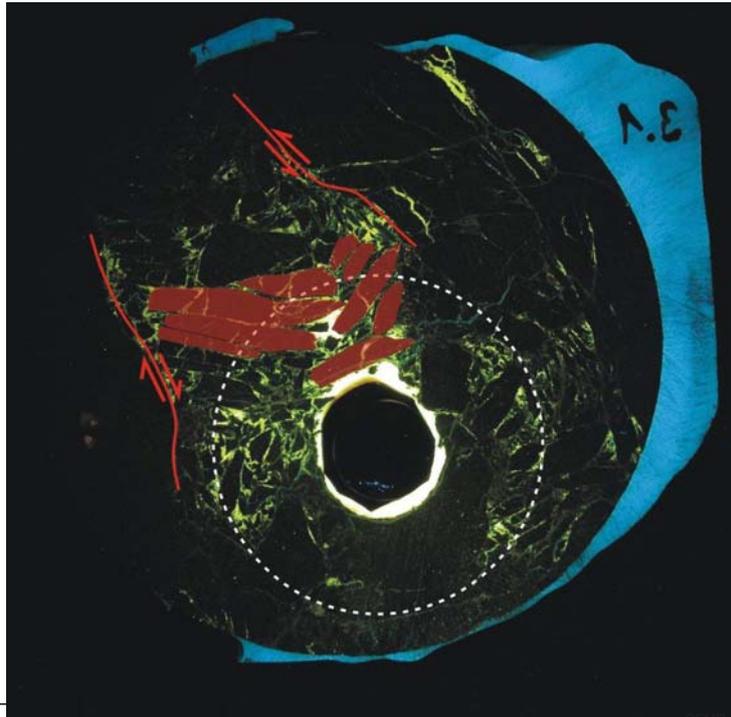


Principal Stress	Magnitude	Trend	Plunge
$\sigma_1$	8.6 MPa	33°	0°
$\sigma_2$	6.7 MPa	123°	70°
$\sigma_3$	3.9 MPa	303°	20°

Principal Stress	Magnitude	Trend	Plunge
$\sigma_1$	6.5 MPa	210°	70°
$\sigma_2$	4.0 MPa	320°	10°
$\sigma_3$	2.2 MPa	50°	15°

- Orientations are derived by breakouts analysis
- Magnitudes are obtained by borehole slotter hydraulic fracturing, over- and undercoring
- Stresses in Opalinus Clay not well constrained
- Different stress field in Opalinus Clay and bounding limestone formations

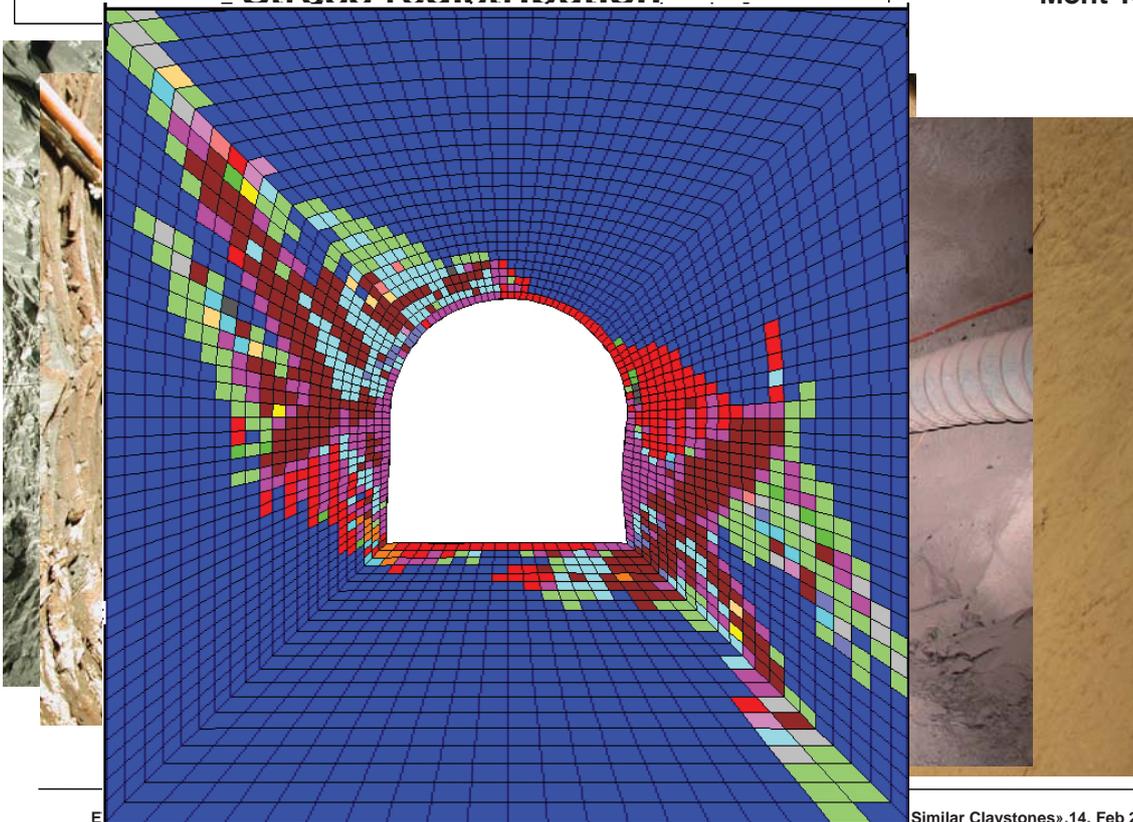
# Borehole closure



ETH Symposium «Rock Mechanics and Rock Engineering of Geological Repositories in Opalinus Clay and Similar Claystones», 14. Feb 2014 CPM, Ecole des Mines Paris, 8.12.05 41



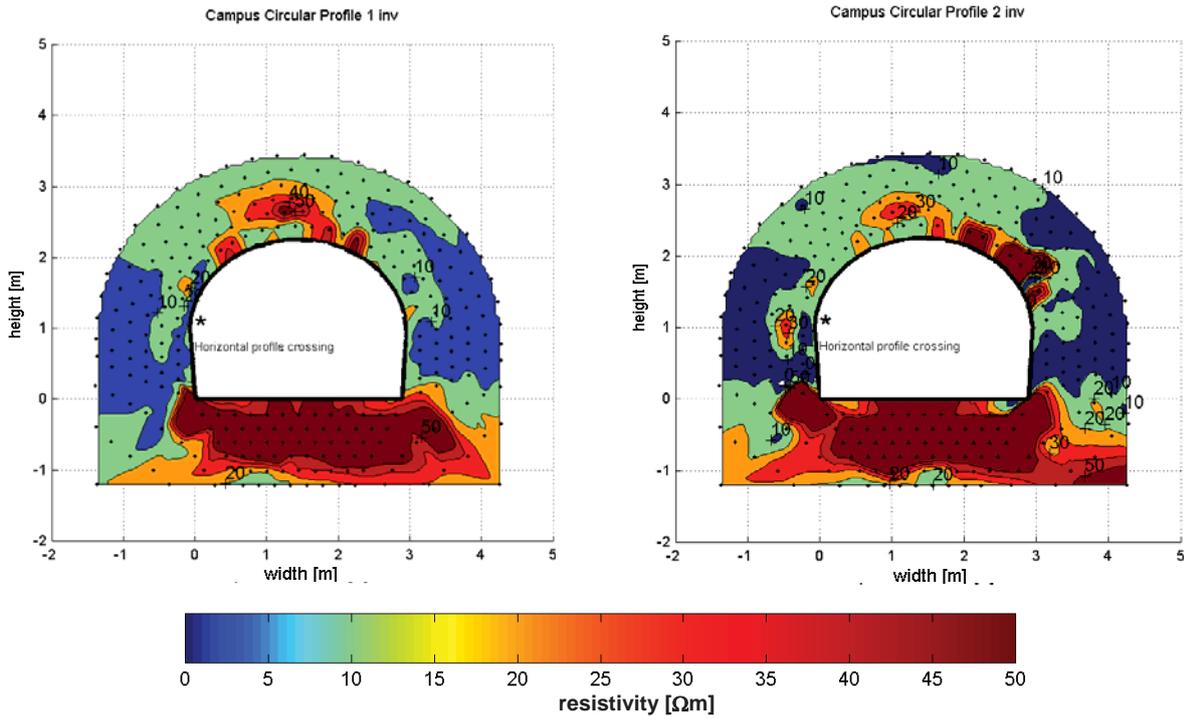
# Stress redistribution



E Similar Claystones», 14. Feb 2014 42



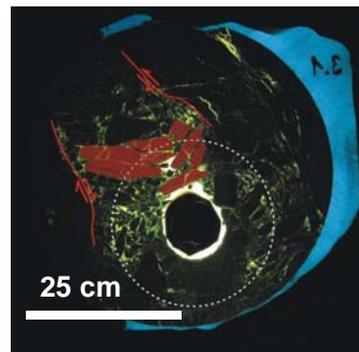
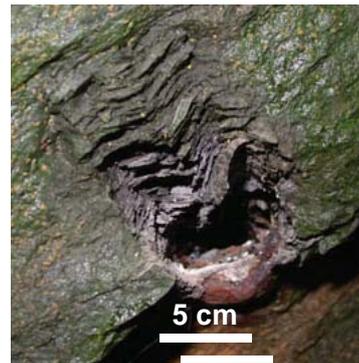
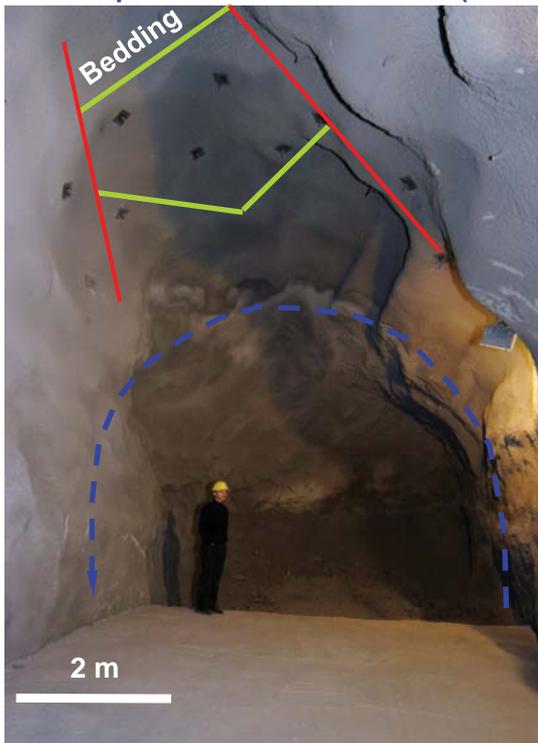
# CAMPUS: Circular Profiles 1 and 2, inversion with cut-off at 50 $\Omega\text{m}$



# Rock mass behaviour: anisotropy Example of breakdown (3 of 4)



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## Rock mechanical variability in the Opalinus-Ton



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Sample orientation	Parameter [unit]	Sandy Facies	Shaly Facies
S P	UCS [MPa]	7 – 22 MPa 7 – 25 MPa	15 MPa 11 MPa
S P	Youngs Modulus [GPa]	0.5 – 19 GPa 2 – 35 GPa	14 GPa 22 GPa
S P	Poissons Ratio	0.05 – 0.4 0.15 – 1	0.25 0.26
Water content		2-5%	6%
Remarks		Very heterogeneous	Best estimates
Authors		After Gschwind (2013)	After Bock (2009)

- No standard approach for conditioning and testing of samples
- Heterogeneous samples of sandy facies cause large variations
- Variable water contents between different datasets, tests should be performed as a function of suction
- No individual test series which comprise the whole range of facies types
- Still only scarce data from the sandy or carbonate-rich facies

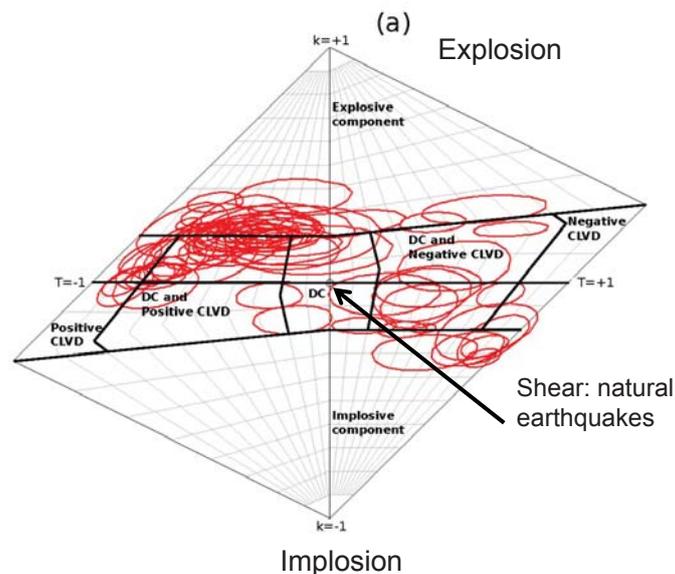


## EZ-G experiment: Spatial location and source mechanisms of microseismic events related to EDZ



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Hudson T-k plot





# Lining: triangular steel arches in FE-A niche

